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मानक

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IS 3075-1 (1986): circlips, Part 1: For shafts [PGD 2: Machine Tool Elements and Holding Devices]



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“Knowledge is such a treasure which cannot be stolen”



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*Indian Standard*

## SPECIFICATION FOR CIRCLIPS

## PART 1 FOR SHAFTS

*( First Revision )***1. Scope**

1.1 Covers the requirement of circlips for shafts of nominal diameter range 3 to 300 mm in normal type and 15 to 100 mm in heavy type.

1.2 Additional information like load-bearing capacity, detachment speed, shape of groove and fitting of circlip have been given in Appendix A.

2. **Symbols** — For the purpose of this standard, the following letter symbols shall apply:

- a* radial width of the lug
- b* beam ( radial width of circlip opposite the aperture )
- c* distance between measuring plates for testing spiral flatness
- $d_1$  shaft diameter
- $d_2$  groove diameter
- $d_3$  internal diameter of circlip not under tension
- $d_4$  maximum symmetrical diameter of bore during fitting
- $d_6$  diameter of the lug holes
- E* modulus of elasticity
- $F_N$  load-bearing capacity of groove at a yield point of the grooved material of 200N/mm<sup>2</sup> ( see A-1.1 )
- $F_R$  load-bearing capacity of circlip with sharp-edged abutment of the pressing part ( see A-1.2 )
- $F_{RG}$  load-bearing capacity of circlip for abutment with edge chamfering distance *g* ( see A-1.2 )
- $R_{eL}$  yield point
- g* edge chamfering distance of the abutment surface to the circlip
- h* distance between the plates when testing conical deformation
- m* groove width
- n* edge margin
- $N_{ds}$  detachment speed of the circlip ( see A-2 )
- r* curvature in the groove base or test jaws
- s* thickness of the circlip
- t* groove depth with nominal sizes of  $d_1$  and  $d_2$

**3. Dimensions, Tolerances and Design Data**

3.1 Dimensions, tolerances and design data for circlips, normal type shall be as given in Table 1, read with Fig. 1.

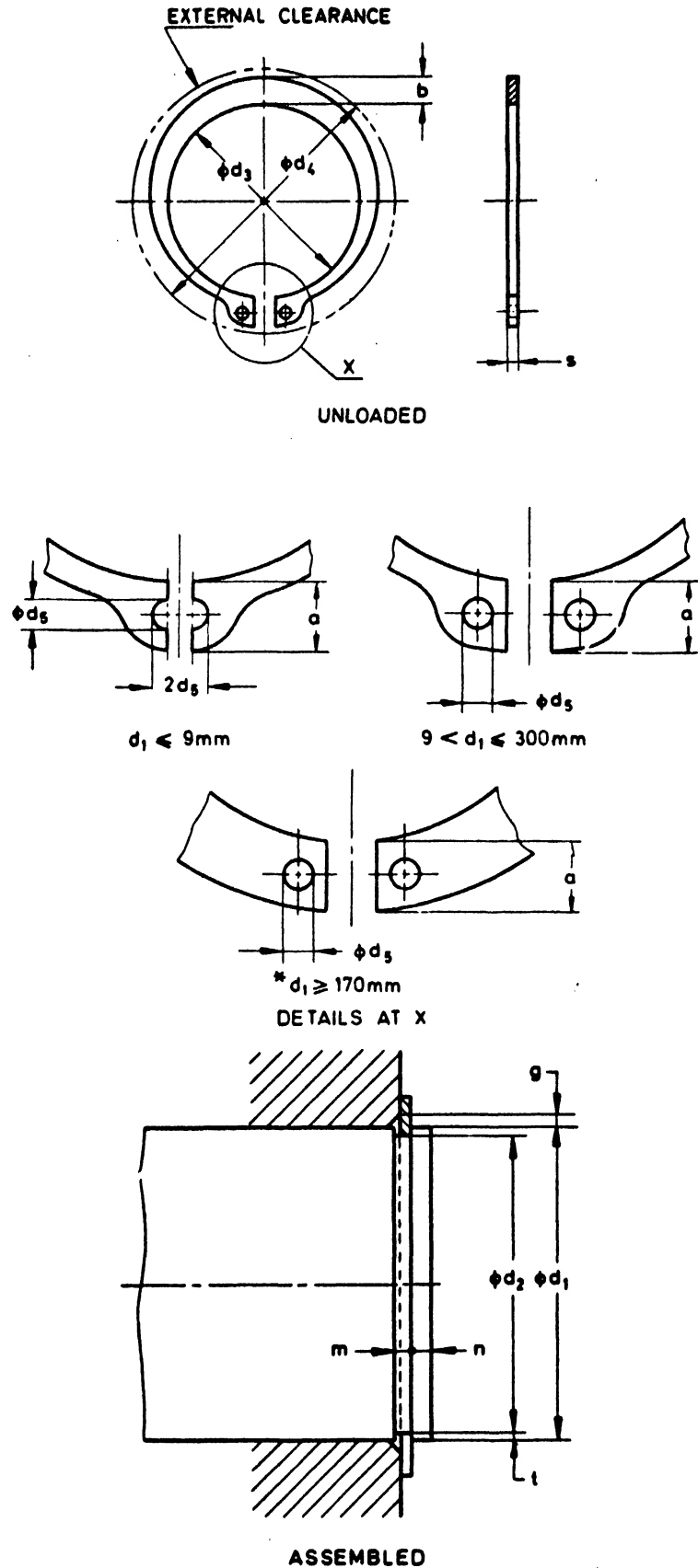
Adopted 25 November 1986

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**IS : 3075 (Part 1) - 1986**

**3.2 Dimensions, tolerances and design data for circlips, heavy type shall be as given in Table 2, read with Fig. 1.**



**Note 1** — Location of the lug hole shall be such that it leaves uniform material all round.  
**Note 2** — Unloaded shape of ring at manufacturer's discretion.

\*At manufacturer's discretion.

**FIG. 1 DIMENSIONS FOR CIRCLIPS — FOR SHAFTS**

**AMENDMENT NO. 1 JUNE 1991  
TO  
IS 3075 ( Part 1 ) : 1986 SPECIFICATION  
FOR CIRCLIPS  
PART 1 FOR SHAFTS**

*( First Revision )*

*( Page 3, Table 1, Tolerance on s for Sizes 5 to 8 ) — Substitute '± 0.03' for the existing.*

*( Page 3, Table 1, Tolerance on d<sub>3</sub> for Nominal Sizes 24 to 32 ) — Substitute '+ 0.21' for the existing.  
- 0.42*

*( Page 3, Table 1, Dimension a for Nominal Size 45 ) — Substitute '6.7' for the existing.*

*( Page 3, Table 1, Dimension d<sub>5</sub> for Nominal Size 42 ) — Substitute '2.5' for the existing*

*( Page 4, Table 1, Tolerance on s for Sizes 72 to 82 ) — Substitute '± 0.06' for the existing.*

*( Page 6, clause 4.2, first line in Hardness column for Sizes Over 48 and Up to 200 ) — Replace '435 by 350' with '435 to 550'.*

**( PE 02 )**

**AMENDMENT NO. 2 NOVEMBER 1997  
TO  
IS 3075 ( PART 1 ) : 1986 SPECIFICATION FOR CIRCLIPS  
PART 1 FOR SHAFTS**

*( First Revision )*

[ Page 6, clause 4.2 ( see also Amendment No. 1 ) ] — Substitute the following table for the existing:

| Nominal Diameter of Circlips |                 | Hardness                                      |
|------------------------------|-----------------|-----------------------------------------------|
| Over                         | Up to Including |                                               |
| —                            | 48              | 480 to 560 HV (corresponding to 48 to 52 HRC) |
| 48                           | 200             | 440 to 510 HV (corresponding to 44 to 49 HRC) |
| 200                          | 300             | 390 to 450 HV (corresponding to 40 to 45 HRC) |

NOTE — Hardness values converted as per IS 4258 : 1982 'Hardness conversion tables for metallic materials (first revision)'.

( Pages 6 and 7, clauses 7.2 to 7.2.2 ) — Substitute the following for the existing clauses:

**7.2 Bend Test and Twist Test**

**7.2.1 Bend test**

The circlip shall be clamped between two jaws, of which one has a radius equal to the thickness of the circlip as shown in Figure 2A. The circlip is bent through 30° by repeated light hammer blows or with a lever, following which there shall be no fracture or cracks in the circlip. The circlip is then further bent until fracture occurs. The fracture surface shall reveal a fine-grained structure.

**7.2.2 Twist test**

The circlip shall be clamped so that 3/4 of its diameter is free as shown in the Figure 2B. An equivalent section of the circlip shall be gripped and rotated through 90° following which there shall be no signs of fracture, cracks or similar defects. The circlips shall then be further twisted in the direction until fracture occurs, following which examination of the fracture shall reveal a uniform grain structure with no sign of lamination or other defects.

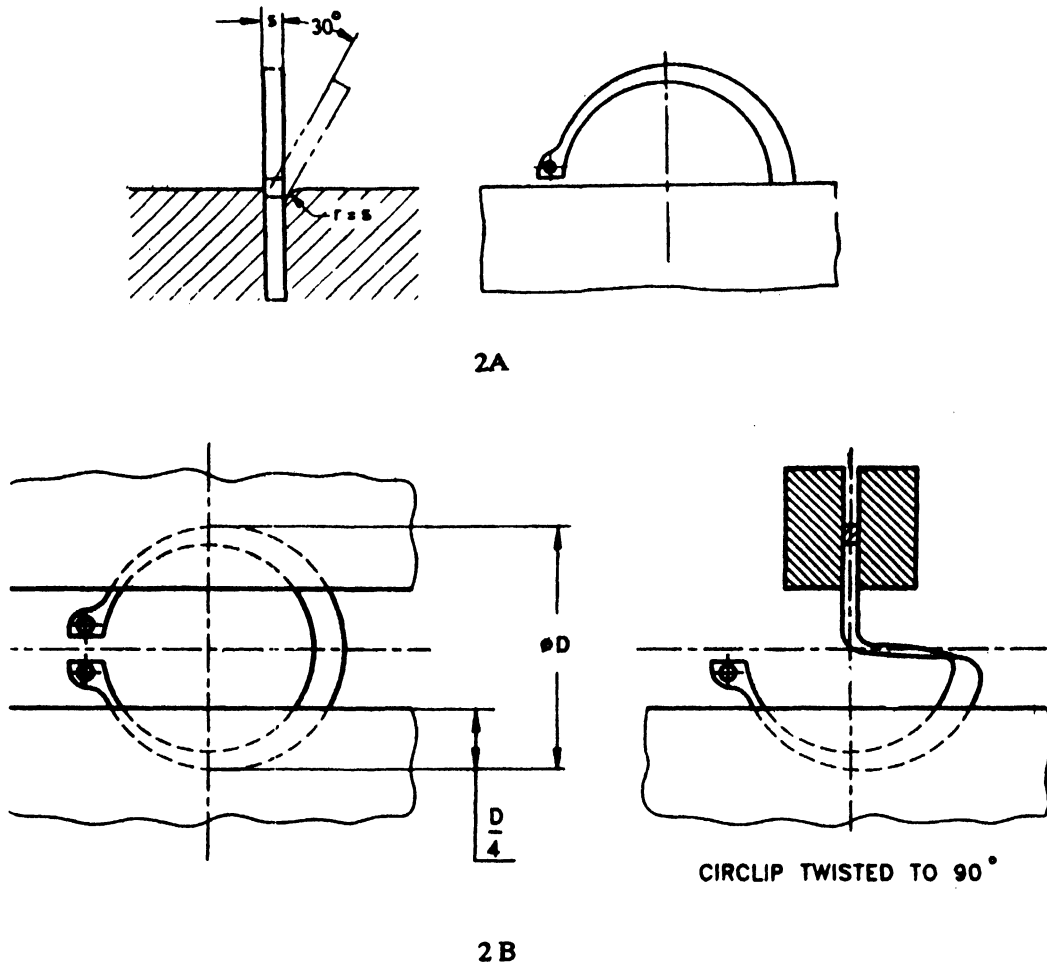


FIG. 2 BEND TEST AND FRACTURE TEST

( Page 7, Fig. 2 ) — Delete.

( PE 02 )



TABLE 1 DIMENSIONS AND DESIGN DATA FOR CIRCLIPS FOR SHAFTS — NORMAL TYPE

( Clause 3.1; and Fig. 1 )

All dimensions in millimetres.

| Shaft Dia, $d_1$<br>Nom. Size | Circlip |           |       |                |     |       | Groove |           |     |       | Design Data§ |      |       |                   |       |     |          |          |                       |
|-------------------------------|---------|-----------|-------|----------------|-----|-------|--------|-----------|-----|-------|--------------|------|-------|-------------------|-------|-----|----------|----------|-----------------------|
|                               | $s$     |           | $d_2$ |                | $a$ | $b^*$ | $d_5$  | $d_3$ †   |     | $m$ ‡ | $t$          | $n$  | $d_4$ | $F_N$             | $F_R$ | $g$ | $F_{Rg}$ | $N_{ds}$ | Nom. Size of<br>Plier |
|                               | Size    | Tolerance | Size  | Tolerance      | Max | Min   | Size   | Tolerance | H13 | Min   | (kN)         | (kN) | (kN)  | Min <sup>-1</sup> |       |     |          |          |                       |
| 3                             | 0.4     | ±0.02     | 2.7   |                | 1.9 | 0.8   | 1      | 2.8       | 0   | 0.5   | 0.1          | 0.3  | 7     | 0.15              | 0.47  | 0.5 | 0.27     | 3 60 000 | 3                     |
| 4                             | 0.4     | ±0.03     | 3.7   | +0.04<br>-0.15 | 2.2 | 0.9   | 1      | 3.8       | 0   | 0.5   | 0.1          | 0.3  | 8.6   | 0.20              | 0.50  | 0.5 | 0.30     | 2 11 000 |                       |
| 5                             | 0.6     | ±0.04     | 4.7   |                | 2.5 | 1.1   | 1      | 4.8       | 0   | 0.7   | 0.1          | 0.3  | 10.3  | 0.26              | 1.00  | 0.5 | 0.80     | 1 54 000 |                       |
| 6                             | 0.7     | ±0.05     | 5.6   |                | 2.7 | 1.3   | 1.2    | 5.7       | 0   | 0.8   | 0.15         | 0.5  | 11.7  | 0.46              | 1.45  | 0.5 | 0.90     | 1 14 000 | 10                    |
| 7                             | 0.8     | ±0.06     | 6.5   | +0.08<br>-0.18 | 3.1 | 1.4   | 1.2    | 6.7       | 0   | 0.9   | 0.15         | 0.5  | 13.5  | 0.54              | 2.60  | 0.5 | 1.40     | 1 21 000 |                       |
| 8                             | 0.8     | ±0.07     | 7.4   |                | 3.2 | 1.5   | 1.2    | 7.6       | 0   | 0.9   | 0.2          | 0.6  | 14.7  | 0.81              | 3.00  | 0.5 | 2.00     | 96 000   |                       |
| 9                             | 1       | ±0.08     | 8.4   |                | 3.3 | 1.7   | 1.2    | 8.6       | 0   | 1.1   | 0.2          | 0.6  | 16    | 0.92              | 3.50  | 0.5 | 2.40     | 85 000   | 19                    |
| 10                            | 1       | ±0.09     | 9.3   |                | 3.3 | 1.8   | 1.5    | 9.6       | 0   | 1.1   | 0.2          | 0.6  | 17    | 1.01              | 4.00  | 1   | 2.40     | 84 000   |                       |
| 11                            | 1       | ±0.10     | 10.2  | +0.10<br>-0.36 | 3.3 | 1.8   | 1.5    | 10.5      | 0   | 1.1   | 0.25         | 0.8  | 18    | 1.40              | 4.50  | 1   | 2.40     | 70 000   |                       |
| 12                            | 1       | ±0.11     | 11    |                | 3.3 | 1.8   | 1.7    | 11.5      | 0   | 1.1   | 0.25         | 0.8  | 19    | 1.53              | 5.00  | 1   | 2.40     | 75 000   | 40                    |
| 13                            | 1       | ±0.12     | 11.9  |                | 3.4 | 2     | 1.7    | 12.4      | 0   | 1.1   | 0.3          | 0.9  | 20.2  | 2.00              | 5.80  | 1   | 2.40     | 66 000   |                       |
| 14                            | 1       | ±0.13     | 12.9  |                | 3.5 | 2.1   | 1.7    | 13.4      | 0   | 1.1   | 0.3          | 0.9  | 21.4  | 2.15              | 6.35  | 1   | 2.40     | 58 000   |                       |
| 15                            | 1       | ±0.14     | 13.8  |                | 3.6 | 2.2   | 1.7    | 14.3      | 0   | 1.1   | 0.35         | 1.1  | 22.6  | 2.66              | 6.90  | 1   | 2.40     | 50 000   | 19                    |
| 16                            | 1       | ±0.15     | 14.7  |                | 3.7 | 2.2   | 1.7    | 15.2      | 0   | 1.1   | 0.4          | 1.2  | 23.6  | 3.26              | 7.40  | 1   | 2.40     | 45 000   |                       |
| 17                            | 1       | ±0.16     | 15.7  |                | 3.8 | 2.3   | 1.7    | 16.2      | 0   | 1.1   | 0.4          | 1.2  | 25    | 3.46              | 8.00  | 1   | 2.40     | 41 000   |                       |
| 18                            | 1.2     | ±0.17     | 16.5  |                | 3.9 | 2.4   | 2      | 17        | 0   | 1.3   | 0.5          | 1.5  | 26.2  | 4.58              | 17.0  | 1.5 | 3.75     | 39 000   | 19                    |
| 19                            | 1.2     | ±0.18     | 17.5  |                | 3.9 | 2.5   | 2      | 18        | 0   | 1.3   | 0.5          | 1.5  | 27.2  | 4.84              | 17.0  | 1.5 | 3.80     | 35 000   |                       |
| 20                            | 1.2     | ±0.19     | 18.5  |                | 4   | 2.6   | 2      | 19        | 0   | 1.3   | 0.5          | 1.5  | 28.4  | 5.06              | 17.1  | 1.5 | 3.85     | 32 000   |                       |
| 21                            | 1.2     | ±0.20     | 19.5  | +0.13<br>-0.42 | 4.1 | 2.7   | 2      | 20        | 0   | 1.3   | 0.5          | 1.5  | 29.6  | 5.36              | 16.8  | 1.5 | 3.75     | 29 000   | 19                    |
| 22                            | 1.2     | ±0.21     | 20.5  |                | 4.2 | 2.8   | 2      | 21        | 0   | 1.3   | 0.5          | 1.5  | 30.8  | 5.65              | 16.9  | 1.5 | 3.80     | 27 000   |                       |
| 24                            | 1.2     | ±0.22     | 22.2  |                | 4.4 | 3     | 2      | 22.9      | 0   | 1.3   | 0.55         | 1.7  | 33.2  | 6.75              | 16.1  | 1.5 | 3.65     | 27 000   |                       |
| 25                            | 1.2     | ±0.23     | 23.2  |                | 4.4 | 3     | 2      | 23.9      | 0   | 1.3   | 0.55         | 1.7  | 34.2  | 7.05              | 16.2  | 1.5 | 3.70     | 25 000   | 19                    |
| 26                            | 1.2     | ±0.24     | 24.2  |                | 4.5 | 3.1   | 2      | 24.9      | 0   | 1.3   | 0.55         | 1.7  | 35.5  | 7.34              | 16.1  | 1.5 | 3.70     | 24 000   |                       |
| 28                            | 1.5     | ±0.25     | 25.9  | +0.41<br>-0.42 | 4.7 | 3.2   | 2      | 26.6      | 0   | 1.6   | 0.7          | 2.1  | 37.9  | 10.00             | 32.1  | 1.5 | 7.50     | 21 200   |                       |
| 29                            | 1.5     | ±0.26     | 26.9  |                | 4.8 | 3.4   | 2      | 27.6      | 0   | 1.6   | 0.7          | 2.1  | 39.1  | 10.37             | 31.8  | 1.5 | 7.45     | 20 000   | 19                    |
| 30                            | 1.5     | ±0.27     | 27.9  |                | 5   | 3.5   | 2      | 28.6      | 0   | 1.6   | 0.7          | 2.1  | 40.5  | 10.73             | 32.1  | 1.5 | 7.65     | 18 900   |                       |
| 32                            | 1.5     | ±0.28     | 29.6  |                | 5.2 | 3.6   | 2.5    | 30.3      | 0   | 1.6   | 0.85         | 2.6  | 43    | 13.85             | 31.2  | 2   | 5.55     | 16 900   |                       |
| 34                            | 1.5     | ±0.29     | 31.5  |                | 5.4 | 3.8   | 2.5    | 31.3      | 0   | 1.6   | 0.85         | 2.6  | 45.4  | 14.72             | 31.3  | 2   | 5.60     | 16 100   | 19                    |
| 35                            | 1.5     | ±0.30     | 32.2  | +0.25<br>-0.5  | 5.6 | 3.9   | 2.5    | 33        | 0   | 1.6   | 1            | 3    | 46.8  | 17.80             | 30.8  | 2   | 5.55     | 15 500   |                       |
| 36                            | 1.75    | ±0.31     | 33.2  |                | 5.6 | 4     | 2.5    | 34        | 0   | 1.85  | 1            | 3    | 47.8  | 18.33             | 49.4  | 2   | 9.00     | 14 500   |                       |
| 38                            | 1.75    | ±0.32     | 35.2  |                | 5.8 | 4.2   | 2.5    | 36        | 0   | 1.85  | 1            | 3    | 50.2  | 19.30             | 49.5  | 2   | 9.10     | 13 600   | 40                    |
| 40                            | 1.75    | ±0.33     | 36.5  |                | 6   | 4.4   | 2.5    | 37.5      | 0   | 1.85  | 1.25         | 3.8  | 52.6  | 25.30             | 51.0  | 2   | 9.50     | 14 300   |                       |
| 42                            | 1.75    | ±0.34     | 38.5  |                | 6.5 | 4.5   | 2      | 39.5      | 0   | 1.85  | 1.25         | 3.8  | 55.7  | 26.70             | 50.0  | 2   | 9.45     | 13 000   |                       |
| 45                            | 1.75    | ±0.35     | 41.5  |                | 5.7 | 4.7   | 2.5    | 42.5      | 0   | 1.85  | 1.25         | 3.8  | 59.1  | 28.60             | 49.0  | 2   | 9.35     | 11 400   | 40                    |
| 48                            | 1.75    | ±0.36     | 44.5  | +0.39<br>-0.9  | 6.9 | 5     | 2.5    | 45.5      | 0   | 1.85  | 1.25         | 3.8  | 62.5  | 30.70             | 49.4  | 2   | 9.55     | 10 300   |                       |
| 50                            | 2       | ±0.37     | 45.8  |                | 6.9 | 5.1   | 2.5    | 47        | 0   | 2.15  | 1.5          | 4.5  | 64.5  | 38.00             | 73.3  | 2   | 14.4     | 10 500   |                       |
| 52                            | 2       | ±0.38     | 47.8  |                | 7   | 5.2   | 2.5    | 49        | 0   | 2.15  | 1.5          | 4.5  | 66.7  | 39.70             | 73.1  | 2.5 | 11.5     | 9 850    | 40                    |
| 55                            | 2       | ±0.39     | 50.8  |                | 7.2 | 5.4   | 2.5    | 52        | 0   | 2.15  | 1.5          | 4.5  | 70.2  | 42.00             | 71.4  | 2.5 | 11.4     | 8 960    |                       |
| 56                            | 2       | ±0.40     | 51.8  |                | 7.3 | 5.5   | 2.5    | 53        | 0   | 2.15  | 1.5          | 4.5  | 71.6  | 42.80             | 70.8  | 2.5 | 11.35    | 8 670    |                       |
| 58                            | 2       | ±0.41     | 53.8  |                | 7.3 | 5.6   | 2.5    | 55        | 0   | 2.15  | 1.5          | 4.5  | 73.6  | 44.30             | 71.1  | 2.5 | 11.5     | 8 200    | 40                    |
| 60                            | 2       | ±0.42     | 55.8  |                | 7.4 | 5.8   | 2.5    | 57        | 0   | 2.15  | 1.5          | 4.5  | 75.6  | 46.00             | 69.2  | 2.5 | 11.3     | 7 620    |                       |
| 62                            | 2       | ±0.43     | 57.8  | +0.46<br>-1.1  | 7.5 | 6     | 2.5    | 59        | 0   | 2.15  | 1.5          | 4.5  | 77.8  | 47.50             | 69.3  | 2.5 | 11.45    | 7 240    |                       |
| 63                            | 2       | ±0.44     | 58.8  |                | 7.6 | 6.2   | 2.5    | 60        | 0   | 2.15  | 1.5          | 4.5  | 79    | 48.30             | 70.2  | 2.5 | 11.6     | 7 050    | 40                    |
| 65                            | 2.5     | ±0.45     | 60.8  |                | 7.8 | 6.3   | 3      | 62        | 0   | 2.65  | 1.5          | 4.5  | 81.4  | 49.80             | 135.6 | 2.5 | 22.7     | 6 640    |                       |
| 68                            | 2.5     | ±0.46     | 63.5  |                | 8   | 6.5   | 3      | 65        | 0   | 2.65  | 1.5          | 4.5  | 84.8  | 52.25             | 135.9 | 2.5 | 23.1     | 6 910    |                       |
| 70                            | 2.5     | ±0.47     | 65.5  |                | 8.1 | 6.6   | 3      | 67        | 0   | 2.65  | 1.5          | 4.5  | 87    | 53.80             | 134.2 | 2.5 | 23.0     | 6 530    |                       |

( Continued )

TABLE 1 DIMENSIONS AND DESIGN DATA FOR CIRCLIPS FOR SHAFTS — NORMAL TYPE — Contd

All dimensions in millimetres.

| Shaft Dia, $d_1$<br>Nom. Size | Circlip |           |       |                 | Groove |      |       |         | Design Data§          |      |      |     |       |       | Nom. Size of Pliers |       |       |            |        |
|-------------------------------|---------|-----------|-------|-----------------|--------|------|-------|---------|-----------------------|------|------|-----|-------|-------|---------------------|-------|-------|------------|--------|
|                               | s       |           | $d_s$ |                 | a      | b*   | $d_5$ | $d_4$ † |                       | m†   | t    | n   | $d_4$ | $F_N$ |                     | $F_B$ | g     | $F_{RB}$   | $Nd_b$ |
|                               | Size    | Tolerance | Size  | Tolerance       | Max    | Min  | Min   | Size    | Tolerance             | H13  | Min  |     | (kN)  | (kN)  |                     |       | (kN)  | $Min^{-1}$ |        |
| 72                            | 2.5     | ± 0.06    | 67.5  | + 0.46<br>- 1.1 | 8.2    | 6.8  | 3     | 69      | 0<br>- 0.3<br>(h 12)  | 2.65 | 1.5  | 4.5 | 89.2  | 55.30 | 131.8               | 2.5   | 22.8  | 6 190      |        |
| 75                            | 2.5     |           | 70.5  |                 | 8.4    | 7    | 3     | 72      |                       | 2.65 | 1.5  | 4.5 | 92.7  | 57.60 | 130.0               | 2.5   | 22.8  | 5 740      |        |
| 78                            | 2.5     |           | 73.5  |                 | 8.6    | 7.3  | 3     | 75      |                       | 2.65 | 1.5  | 4.5 | 96.1  | 60.00 | 131.3               | 3     | 19.75 | 5 450      |        |
| 80                            | 2.5     |           | 74.5  |                 | 8.6    | 7.4  | 3     | 76.5    |                       | 2.65 | 1.75 | 5.3 | 98.1  | 71.60 | 128.4               | 3     | 19.5  | 6 100      |        |
| 82                            | 2.5     | ± 0.07    | 76.5  | + 0.54<br>- 1.3 | 8.7    | 7.6  | 3     | 78.5    | 0<br>- 0.35<br>(h 12) | 2.65 | 1.75 | 5.3 | 100.3 | 73.50 | 128.0               | 3     | 19.6  | 5 860      |        |
| 85                            | 3       |           | 79.5  |                 | 8.7    | 7.8  | 3.5   | 81.5    |                       | 3.15 | 1.75 | 5.3 | 103.3 | 76.20 | 215.4               | 3     | 33.4  | 5 710      |        |
| 88                            | 3       | ± 0.08    | 82.5  | + 0.63<br>- 1.5 | 8.8    | 8    | 3.5   | 84.5    | 0<br>- 0.63<br>(h 13) | 3.15 | 1.75 | 5.3 | 106.5 | 79.00 | 221.8               | 3     | 34.85 | 5 200      |        |
| 90                            | 3       |           | 84.5  |                 | 8.8    | 8.2  | 3.5   | 86.5    |                       | 3.15 | 1.75 | 5.3 | 108.5 | 80.80 | 217.2               | 3     | 34.4  | 4 980      |        |
| 95                            | 3       |           | 89.5  |                 | 9.4    | 8.6  | 3.5   | 91.5    |                       | 3.15 | 1.75 | 5.3 | 114.8 | 85.50 | 212.2               | 3.5   | 29.25 | 4 550      |        |
| 100                           | 3       |           | 94.5  |                 | 9.6    | 9    | 3.5   | 96.5    |                       | 3.15 | 1.75 | 5.3 | 120.2 | 90.00 | 206.4               | 3.5   | 29.0  | 4 180      |        |
| 105                           | 4       | ± 0.09    | 98    | + 0.72<br>- 1.7 | 9.9    | 9.3  | 3.5   | 101     | 0<br>- 0.72<br>(h 13) | 4.15 | 2    | 6   | 125.8 | 107.6 | 471.8               | 3.5   | 67.7  | 4 740      |        |
| 110                           | 4       |           | 103   |                 | 10.1   | 9.6  | 3.5   | 106     |                       | 4.15 | 2    | 6   | 131.2 | 113.0 | 457.0               | 3.5   | 66.9  | 4 340      |        |
| 115                           | 4       | ± 0.09    | 108   | + 0.8<br>- 2    | 10.6   | 9.8  | 3.5   | 111     | 0<br>- 0.81<br>(h 13) | 4.15 | 2    | 6   | 137.3 | 118.2 | 438.6               | 3.5   | 65.5  | 3 970      |        |
| 120                           | 4       |           | 113   |                 | 11     | 10.2 | 3.5   | 116     |                       | 4.15 | 2    | 6   | 143.1 | 123.5 | 424.6               | 3.5   | 64.5  | 3 685      |        |
| 125                           | 4       |           | 118   |                 | 11.4   | 10.4 | 4     | 121     |                       | 4.15 | 2    | 6   | 149   | 128.7 | 411.5               | 4     | 56.5  | 3 420      |        |
| 130                           | 4       |           | 123   |                 | 11.6   | 10.7 | 4     | 126     |                       | 4.15 | 2    | 6   | 154.4 | 134.0 | 395.5               | 4     | 55.2  | 3 180      |        |
| 135                           | 4       | ± 0.09    | 128   | + 0.83<br>- 1.5 | 11.8   | 11   | 4     | 131     | 0<br>- 0.63<br>(h 13) | 4.15 | 2    | 6   | 159.8 | 139.2 | 389.5               | 4     | 55.4  | 2 950      |        |
| 140                           | 4       |           | 133   |                 | 12     | 11.2 | 4     | 136     |                       | 4.15 | 2    | 6   | 165.2 | 144.5 | 376.5               | 4     | 54.4  | 2 760      |        |
| 145                           | 4       | ± 0.09    | 138   | + 0.72<br>- 1.7 | 12.2   | 11.5 | 4     | 141     | 0<br>- 0.72<br>(h 13) | 4.15 | 2    | 6   | 170.6 | 149.6 | 367.0               | 4     | 53.8  | 2 600      |        |
| 150                           | 4       |           | 142   |                 | 13     | 11.8 | 4     | 145     |                       | 4.15 | 2.5  | 7.5 | 177.3 | 193.0 | 357.5               | 4     | 53.4  | 2 480      |        |
| 155                           | 4       |           | 146   |                 | 13     | 12   | 4     | 150     |                       | 4.15 | 2.5  | 7.5 | 182.3 | 199.6 | 352.9               | 4     | 52.6  | 2 710      |        |
| 160                           | 4       |           | 151   |                 | 13.3   | 12.2 | 4     | 155     |                       | 4.15 | 2.5  | 7.5 | 188   | 206.1 | 349.2               | 4     | 52.2  | 2 540      |        |
| 165                           | 4       | ± 0.09    | 155.5 | + 0.8<br>- 2    | 13.5   | 12.5 | 4     | 160     | 0<br>- 0.63<br>(h 13) | 4.15 | 2.5  | 7.5 | 193.4 | 212.5 | 345.3               | 5     | 41.4  | 2 520      |        |
| 170                           | 4       |           | 160.5 |                 | 13.5   | 12.9 | 4     | 165     |                       | 4.15 | 2.5  | 7.5 | 198.4 | 219.1 | 349.2               | 5     | 41.9  | 2 440      |        |
| 175                           | 4       | ± 0.09    | 165.5 | + 0.72<br>- 1.7 | 13.5   | 12.9 | 4     | 170     | 0<br>- 0.72<br>(h 13) | 4.15 | 2.5  | 7.5 | 203.4 | 225.5 | 340.1               | 5     | 40.7  | 2 300      |        |
| 180                           | 4       |           | 170.5 |                 | 14.2   | 13.5 | 4     | 175     |                       | 4.15 | 2.5  | 7.5 | 210   | 232.2 | 345.3               | 5     | 41.4  | 2 180      |        |
| 185                           | 4       |           | 175.5 |                 | 14.2   | 13.5 | 4     | 180     |                       | 4.15 | 2.5  | 7.5 | 215   | 238.6 | 336.7               | 5     | 40.4  | 2 070      |        |
| 190                           | 4       |           | 180.5 |                 | 14.2   | 14   | 4     | 185     |                       | 4.15 | 2.5  | 7.5 | 220   | 245.1 | 333.8               | 5     | 40.0  | 1 970      |        |
| 195                           | 4       | ± 0.09    | 185.5 | + 0.8<br>- 2    | 14.2   | 14   | 4     | 190     | 0<br>- 0.81<br>(h 13) | 4.15 | 2.5  | 7.5 | 225   | 251.8 | 325.4               | 5     | 39.0  | 1 835      |        |
| 200                           | 4       |           | 190.5 |                 | 14.2   | 14   | 4     | 195     |                       | 4.15 | 2.5  | 7.5 | 230   | 258.3 | 319.2               | 5     | 38.3  | 1 770      |        |
| 210                           | 5       | ± 0.09    | 198   | + 0.72<br>- 1.7 | 14.2   | 14   | 4     | 204     | 0<br>- 0.72<br>(h 13) | 5.15 | 3    | 9   | 240   | 325.1 | 598.2               | 6     | 59.9  | 1 835      |        |
| 220                           | 5       |           | 208   |                 | 14.2   | 14   | 4     | 214     |                       | 5.15 | 3    | 9   | 250   | 340.8 | 572.4               | 6     | 57.3  | 1 620      |        |
| 230                           | 5       |           | 218   |                 | 14.2   | 14   | 4     | 224     |                       | 5.15 | 3    | 9   | 260   | 356.6 | 548.9               | 6     | 55.0  | 1 445      |        |
| 240                           | 5       |           | 228   |                 | 14.2   | 14   | 4     | 234     |                       | 5.15 | 3    | 9   | 270   | 372.6 | 530.3               | 6     | 53.0  | 1 305      |        |
| 250                           | 5       | ± 0.09    | 238   | + 0.8<br>- 2    | 14.2   | 14   | 4     | 244     | 0<br>- 0.81<br>(h 13) | 5.15 | 3    | 9   | 280   | 388.3 | 504.3               | 6     | 50.5  | 1 180      |        |
| 260                           | 5       |           | 245   |                 | 16.2   | 16   | 5     | 252     |                       | 5.15 | 4    | 12  | 294   | 535.8 | 540.6               | 6     | 54.6  | 1 320      |        |
| 270                           | 5       | ± 0.09    | 255   | + 0.8<br>- 2    | 16.2   | 16   | 5     | 262     | 0<br>- 0.81<br>(h 13) | 5.15 | 4    | 12  | 304   | 556.6 | 525.3               | 6     | 52.5  | 1 215      |        |
| 280                           | 5       |           | 265   |                 | 16.2   | 16   | 5     | 272     |                       | 5.15 | 4    | 12  | 314   | 576.6 | 508.2               | 6     | 50.9  | 1 100      |        |
| 290                           | 5       |           | 275   |                 | 16.2   | 16   | 5     | 282     |                       | 5.15 | 4    | 12  | 324   | 599.1 | 490.8               | 6     | 49.2  | 1 005      |        |
| 300                           | 5       |           | 285   |                 | 16.2   | 16   | 5     | 292     |                       | 5.15 | 4    | 12  | 334   | 619.1 | 475.0               | 6     | 47.5  | 930        |        |

\*Dimension b shall not exceed dimension a Max.

†See A-3.1.

‡See A-3.2.

§The design data apply only to circlips of spring steel as per IS : 2507-1975 'Specification for cold rolled steel strips for spring ( first revision )',  $d_4$  is calculated from  $d_4 = d_1 + 2.1 a$ .

||Pliers conforming to IS : 7990-1976 'Specification for pliers for external circlips'.

TABLE 2 DIMENSIONS AND DESIGN DATA FOR CIRCLIPS FOR SHAFTS — HEAVY TYPE

( Clause 3.2 and Fig. 1 )

All dimensions in millimetres.

| Shaft Dia, $d_1$<br>Nom. Size | Circlip |            |       |           |      |           | Groove |         |           |       | Design Data§ |     |       |       |       |      | Nom. Size of<br>Pliers |            |          |
|-------------------------------|---------|------------|-------|-----------|------|-----------|--------|---------|-----------|-------|--------------|-----|-------|-------|-------|------|------------------------|------------|----------|
|                               | s       |            | $d_s$ |           | a    | $b^*$     | $d_5$  | $d_3$ † |           | $m$ ‡ | t            | n   | $d_4$ | $F_N$ | $F_R$ | g    |                        | $F_{RG}$   | $N_{ds}$ |
|                               | Size    | Tolerance  | Size  | Tolerance | Max  | $\approx$ | Min    | Size    | Tolerance | H13   |              | Min | (kN)  | (kN)  |       | (kN) |                        | $Min^{-1}$ |          |
|                               |         |            |       |           |      |           |        |         |           |       |              |     |       |       |       |      |                        |            |          |
| 15                            | 1.5     |            | 13.8  |           | 4.8  | 2.4       | 2      | 14.3    | 0         | 1.6   | 0.35         | 1.1 | 25.1  | 2.66  | 15.5  | 1    | 6.40                   | 57 000     |          |
| 16                            | 1.5     |            | 14.7  |           | 5    | 2.5       | 2      | 15.2    | 0         | 1.6   | 0.4          | 1.2 | 26.5  | 3.26  | 16.6  | 1    | 6.35                   | 44 000     |          |
| 17                            | 1.5     |            | 15.7  | +0.10     | 5    | 2.6       | 2      | 16.2    | -0.11     | 1.6   | 0.4          | 1.2 | 27.5  | 3.46  | 18.0  | 1    | 6.70                   | 46 000     |          |
| 18                            | 1.5     |            | 16.5  | -0.36     | 5.1  | 2.7       | 2      | 17      | (h 11)    | 1.6   | 0.5          | 1.5 | 28.7  | 4.58  | 26.6  | 1.5  | 5.85                   | 42 750     |          |
| 20                            | 1.75    | $\pm$ 0.05 | 18.5  | +0.13     | 5.5  | 3         | 2      | 19      | 0         | 1.85  | 0.5          | 1.5 | 31.6  | 5.06  | 36.3  | 1.5  | 8.20                   | 36 000     |          |
| 22                            | 1.75    |            | 20.5  | -0.42     | 6    | 3.1       | 2      | 21      | -0.13     | 1.85  | 0.5          | 1.5 | 34.6  | 5.65  | 36.0  | 1.5  | 8.10                   | 29 000     |          |
| 24                            | 1.75    |            | 22.2  |           | 6.3  | 3.2       | 2      | 22.9    | (h 11)    | 1.85  | 0.55         | 1.7 | 37.3  | 6.75  | 34.2  | 1.5  | 7.60                   | 29 200     |          |
| 25                            | 2       |            | 23.2  |           | 6.4  | 3.4       | 2      | 23.9    | 0         | 2.15  | 0.55         | 1.7 | 38.5  | 7.05  | 45.0  | 1.5  | 10.3                   | 25 000     |          |
| 28                            | 2       |            | 25.9  | +0.21     | 6.5  | 3.5       | 2      | 26.6    | -0.21     | 2.15  | 0.7          | 2.1 | 41.7  | 10.0  | 57.0  | 1.5  | 13.4                   | 22 200     |          |
| 30                            | 2       |            | 27.9  | -0.42     | 6.5  | 4.1       | 2      | 28.6    | (h 12)    | 2.15  | 0.7          | 2.1 | 43.7  | 10.7  | 57.0  | 1.5  | 13.6                   | 21 100     |          |
| 32                            | 2       |            | 29.6  |           | 6.5  | 4.1       | 2.5    | 30.3    |           | 2.15  | 0.85         | 2.6 | 45.7  | 13.8  | 55.5  | 2    | 10.0                   | 18 400     |          |
| 34                            | 2.5     |            | 31.5  |           | 6.6  | 4.2       | 2.5    | 32.3    |           | 2.65  | 0.85         | 2.6 | 47.9  | 14.7  | 87.0  | 2    | 15.6                   | 17 800     |          |
| 35                            | 2.5     | $\pm$ 0.06 | 32.2  | +0.25     | 6.7  | 4.2       | 2.5    | 33      |           | 2.65  | 1            | 3   | 49.1  | 17.8  | 86.0  | 2    | 15.4                   | 16 500     |          |
| 38                            | 2.5     |            | 35.2  | -0.5      | 6.8  | 4.3       | 2.5    | 36      |           | 2.65  | 1            | 3   | 52.3  | 19.3  | 101   | 2    | 18.6                   | 14 500     |          |
| 40                            | 2.5     |            | 36.5  |           | 7    | 4.4       | 2.5    | 37.5    | 0         | 2.65  | 1.25         | 3.8 | 54.7  | 25.3  | 104   | 2    | 19.3                   | 14 300     |          |
| 42                            | 2.5     |            | 38.5  |           | 7.2  | 4.5       | 2.5    | 39.5    | -0.25     | 2.65  | 1.25         | 3.8 | 57.2  | 26.7  | 102   | 2    | 19.2                   | 13 000     |          |
| 45                            | 2.5     |            | 41.5  | +0.39     | 7.5  | 4.7       | 2.5    | 42.5    | (h 12)    | 2.65  | 1.25         | 3.8 | 60.8  | 28.6  | 100   | 2    | 19.1                   | 11 400     |          |
| 48                            | 2.5     |            | 44.5  | -0.9      | 7.8  | 5         | 2.5    | 45.5    |           | 2.65  | 1.25         | 3.8 | 64.4  | 30.7  | 101   | 2    | 19.5                   | 10 300     |          |
| 50                            | 3       |            | 45.8  |           | 8    | 5.1       | 2.5    | 47      |           | 3.15  | 1.5          | 4.5 | 66.8  | 38.0  | 165   | 2    | 32.4                   | 10 500     |          |
| 52                            | 3       |            | 47.8  |           | 8.2  | 5.2       | 2.5    | 49      |           | 3.15  | 1.5          | 4.5 | 69.3  | 39.7  | 165   | 2.5  | 26.0                   | 9 850      |          |
| 55                            | 3       | $\pm$ 0.07 | 50.8  |           | 8.5  | 3.4       | 2.5    | 52      |           | 3.15  | 1.5          | 4.5 | 72.9  | 42.0  | 161   | 2.5  | 25.6                   | 8 960      |          |
| 58                            | 3       |            | 53.8  |           | 8.8  | 5.6       | 2.5    | 55      |           | 3.15  | 1.5          | 4.5 | 76.5  | 44.3  | 160   | 2.5  | 26.0                   | 8 200      |          |
| 60                            | 3       |            | 55.8  |           | 9    | 5.8       | 2.5    | 57      |           | 3.15  | 1.5          | 4.5 | 78.9  | 46.0  | 156   | 2.5  | 25.4                   | 7 620      |          |
| 65                            | 4       |            | 60.8  |           | 9.3  | 6.3       | 3      | 62      | 0         | 4.15  | 1.5          | 4.5 | 84.5  | 49.8  | 346   | 2.5  | 58.0                   | 6 640      |          |
| 70                            | 4       |            | 65.5  | +0.46     | 9.5  | 6.6       | 3      | 67      | -0.30     | 4.15  | 1.5          | 4.5 | 90    | 53.8  | 343   | 2.5  | 59.0                   | 6 530      |          |
| 75                            | 4       |            | 70.5  | -1.1      | 9.7  | 7         | 3      | 72      | (h 12)    | 4.15  | 1.5          | 4.5 | 95.4  | 57.6  | 333   | 2.5  | 58.0                   | 5 740      |          |
| 80                            | 4       |            | 74.5  |           | 9.8  | 7.4       | 3      | 76.5    |           | 4.15  | 1.75         | 5.3 | 100.6 | 71.6  | 328   | 3    | 50.0                   | 6 100      |          |
| 85                            | 4       | $\pm$ 0.08 | 79.5  |           | 10   | 7.8       | 3.5    | 81.5    | 0         | 4.15  | 1.75         | 5.3 | 106   | 76.2  | 383   | 3    | 59.4                   | 5 710      |          |
| 90                            | 4       |            | 84.5  | +0.54     | 10.2 | 8.2       | 3.5    | 86.5    | -0.35     | 4.15  | 1.75         | 5.3 | 111.5 | 80.8  | 386   | 3    | 61.0                   | 4 980      |          |
| 100                           | 4       |            | 94.5  | -1.3      | 10.5 | 9         | 3.5    | 96.5    | (h 12)    | 4.15  | 1.75         | 5.3 | 122.1 | 90.0  | 368   | 3.5  | 51.6                   | 4 180      |          |

\*Dimension b shall not exceed dimension a Max.

†See A-3.1.

‡See A-3.2.

§The design data apply to circlips of spring steel as per IS : 2507-1975,  $b_4$  is calculated from  $d_4 = d_1 + 2.1 a$ .

||Pliers conforming to IS : 7990-1976.

## IS : 3075 ( Part 1 ) - 1986

### 4. Material and Hardness

4.1 The circlips shall be manufactured from spring steel such as 70 C6 or 75 C6 as per IS : 2507-1975 'Specification for cold rolled steel strips for springs ( first revision )'.

4.2 Hardness of circlips shall be as given below:

| Nominal Diameter of Circlips |       | Hardness                                                                    |
|------------------------------|-------|-----------------------------------------------------------------------------|
| Over                         | Up to |                                                                             |
| —                            | 48    | 470 to 580 Vickers hardness (corresponding to 47 to 54 Rockwell C hardness) |
| 48                           | 200   | 435 to 350 Vickers hardness (corresponding to 44 to 51 Rockwell C hardness) |
| 200                          | 300   | 390 to 470 Vickers hardness (corresponding to 40 to 47 Rockwell C hardness) |

**Note** — Hardness values converted as per IS : 4258-1982 'Hardness conversion Table for metallic materials ( first revision )'.

### 5. Designation

5.1 A circlip for shaft diameter ( nominal size )  $d_1 = 40$  mm and thickness 1.75 mm, normal type (N), shall be designated as:

Circlip 40 × 1.75 N IS : 3075 ( Part 1 )

5.2 A circlip for shaft diameter ( nominal size )  $d_1 = 40$  mm and thickness 2.5 mm, heavy type (H), shall be designated as:

Circlip 40 × 2.5 H IS : 3075 ( Part 1 )

### 6. Finish

6.1 All sharp edges shall be removed from the circlips. The circlips shall be free from burrs, cracks, laminations and other defects.

6.1.1 The maximum permissible deviation on the profile at engaging lip may also be mutually agreed upon between the manufacturer and the user in case of special application.

6.2 Unless any alternative finish is specified by the purchaser, the circlips shall be chemically and/or thermally blackened or phosphated to class A2 of IS : 3618-1966 'Phosphate treatment for iron and steel for protection against corrosion'. The coated circlips shall be subjected to appropriate treatment to avoid hydrogen embrittlement.

**Note** — In the case of circlips with electroplated surface protection, the upper limit of the circlips thickness  $S$  may be exceeded according to the film thickness of the plating required. This shall be taken into account in the design of the groove.

### 7. Tests

#### 7.1 Testing of Material

7.1.1 Vickers hardness test in accordance with IS : 1501 ( Part 1 )-1984 'Method for Vickers hardness test for metallic materials: Part 1 HV 5 to HV 100 ( second revision )'.

7.1.2 Rockwell hardness test in accordance with IS : 1586-1968 'Methods for Rockwell hardness test ( B and C scales ) for steels ( first revision )'.

**Note 1** — In case of doubt, the Vickers hardness test applies.

**Note 2** — In case of circlips, the hardness test is regarded as a destructive test.

#### 7.2 Bend Test and Fracture Test

7.2.1 The testing of the circlip for ductility shall be carried out in accordance with Fig. 2.

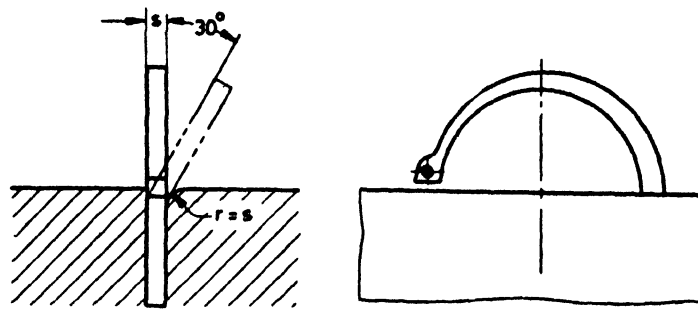


FIG. 2 BEND TEST AND FRACTURE TEST

7.2.2 One half of the circlip is clamped between two jaws, of which one has a radius equal to the thickness of the circlip. The circlip is bent through 30° by repeated light hammer blows or with a lever, following which there shall be no fracture or cracks in the circlip. The circlip is then further bent until fracture occurs. The fracture surface shall reveal a fine-grained structure.

7.3 Deformation Test

7.3.1 Testing the conical deformation — The circlip is placed between two parallel plates and loaded in accordance with Fig. 3. The distance  $h - s$  measured under force  $F$  shall not exceed the maximum value stated as given in Table 3.

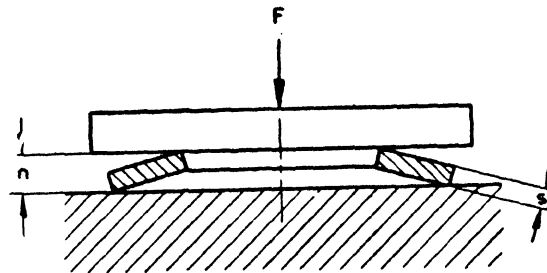


FIG. 3 TESTING CONICAL DEFORMATION

TABLE 3 TESTING THE CONICAL DEFORMATION

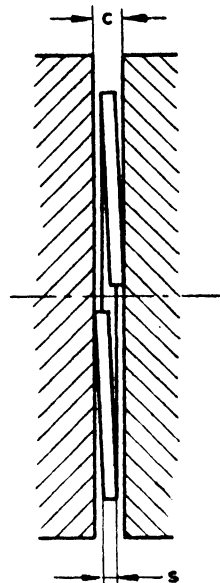
( Clause 7.3.1; and Fig. 3 )

All dimensions in millimetres.

| Nominal Diameter of Circlips |       | Force $F$ in N<br>$\pm 5\%$ |            | $h - s$<br>Max  |
|------------------------------|-------|-----------------------------|------------|-----------------|
| Over                         | Up to | Normal Type                 | Heavy Type |                 |
| —                            | 22    | 30                          | 60         | $b \times 0.03$ |
| 22                           | 38    | 40                          | 80         |                 |
| 38                           | 82    | 60                          | 120        |                 |
| 82                           | 150   | 80                          | 160        | $b \times 0.02$ |
| 150                          | 300   | 150                         | 300        |                 |

7.3.2 Testing the spiral flatness

7.3.2.1 The circlip shall fall through two parallel planes with a clearance  $c$  as given in table below ( read with Fig. 4 ):



| Nominal Diameter of Circlips |       | $c$            |
|------------------------------|-------|----------------|
| Over                         | Up to |                |
| —                            | 100   | $1.5 \times s$ |
| 100                          | —     | $1.8 \times s$ |

FIG. 4 TESTING SPIRAL FLATNESS

7.4 Testing the Function ( Permanent Set and Grip Test )

7.4.1 The circlip is passed five times over a cone with a diameter of  $1.01 d_1$  in accordance with Fig. 12 ( see A-4 ) and then be fitted on to a shaft of minimum groove diameter  $d_2$ , where it shall remain under its own weight.

7.5 Acceptance Testing

7.5.1 Table 4 applies to features, while Table 5 applies for the acceptance quality level (AQL).

TABLE 4 FEATURES FOR ACCEPTANCE TESTS

| Features                                                                                                                            |
|-------------------------------------------------------------------------------------------------------------------------------------|
| Circlips thickness, $s$<br>Circlips internal diameter, $d_s$<br>Conical deformation<br>Spiral flatness<br>Function ( set and grip ) |

TABLE 5 ACCEPTABLE QUALITY LEVEL

| Acceptable Quality Level, AQL* |                             |
|--------------------------------|-----------------------------|
| For Testing of Features        | For Testing of Faulty Parts |
| 1                              | 1.5                         |

\*Refer IS : 2500 ( Part 1 )-1973 'Sampling inspection tables: Part 1 Inspection by attributes and by count of defects ( first revision )'.

## 8. Preservation and Packing

**8.1** A suitable anti-corrosive surface treatment shall be given to the circlips for protection during transit.

**8.2 Packing** — Unless otherwise specified, the circlips shall be packed in cartons of 100, 500 and 1000 or multiples thereof. Each carton shall contain circlips of one size only.

## 9. Marking

**9.1** The label on the carton shall carry the designation, number of pieces and the manufacturer's name or trade-mark.

**9.2 Standard Mark** — Details available with Bureau of Indian Standards.

## APPENDIX A

( Clause 1.2 )

### ADDITIONAL INFORMATION FOR LOAD BEARING CAPACITY, DETACHMENT SPEED, SHAPE OF GROOVE AND FITTING OF CIRCLIPS

**A-1. Load-Bearing Capacity**— A circlip connection requires separate calculations for the load bearing capacity of the groove  $F_N$  and for the load-bearing capacity of the circlip  $F_R$ . In each case the weaker part is that which applies. The load-bearing capacities ( $F_N$ ,  $F_R$ ,  $F_{Rg}$ ) given in 3, contain no safety, neither against yielding under static stress nor against fatigue fracture under fluctuating stress. There shall be at least twice the level of safety against fracture under static stress.

**A-1.1 Load-Bearing Capacity of Groove,  $F_N$**  — The load-bearing capacity of the groove  $F_N$  in 3, applies for a yield point of the material in the region of the shaft groove of  $R_{eL} = 200 \text{ N/mm}^2$  as well as for the given nominal groove depths  $t$  and edge margins  $n$ .

The load-bearing capacity  $F'_N$  for deviating groove depths  $t'$  (resulting from deviating shaft diameters  $d_1$  and/or deviating groove diameters  $d_2$ ) and yield points  $R'_{eL}$  is directly proportional to the groove depth and the yield:

$$F'_N = F_N \cdot \frac{t'}{t} \cdot \frac{R'_{eL}}{200}$$

**A-1.2 Load-Bearing Capacity of Circlip,  $F_R$**  — The load-bearing capacity of the circlip  $F_R$  in accordance with 3 applies to a sharp-edged abutment of the pressing machine part ( see Fig. 5 ).

The values  $F_{Rg}$  apply to an abutment with an edge chamfering distance  $g$  ( see Fig. 6 ). The two values  $F_R$  and  $F_{Rg}$  apply to circlip materials with a modulus of elasticity ( E-modulus ) of  $210\,000 \text{ N/mm}^2$ . If circlips of a different material with a different E modulus  $E'$  are used, then, for conversion, the load-bearing capacity of the circlip is directly proportional to the modulus of elasticity:

$$F'_R = F_R \cdot \frac{E'}{210\,000}, \text{ and}$$

$$F'_{Rg} = F_{Rg} \cdot \frac{E'}{210\,000}$$

If the existing edge chamfering distance  $g'$  deviates from the values in 3, then, for conversion, the load-bearing capacity of the circlip is indirectly proportional to the edge chamfering distance:

$$F'_{Rg} = F_{Rg} \cdot \frac{g}{g'}$$

**Note** — If  $F'_{Rg}$  with small values of  $g'$  is greater than  $F_R$ , then  $F_R$  applies.

If the existing forces, because of too great an edge chamfering distance cannot be accommodated, then a sharp-edged abutment shall be created by means of a supporting ring ( see Fig. 7 ).

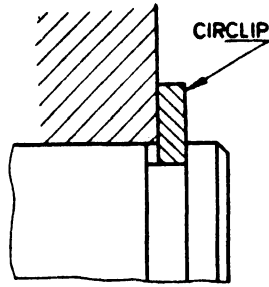


FIG. 5 SHARP EDGE ABUTMENT

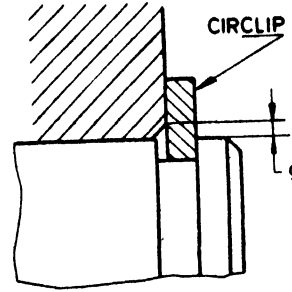


FIG. 6 ABUTMENT WITH EDGE CHAMFERING DISTANCE (CHAMFERING OR ROUNDING)

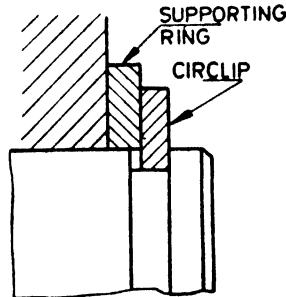


FIG. 7 SHARP EDGE ABUTMENT WITH SUPPORTING RING

**A-2. Detachment Speed,  $N_{ds}$**  — The application of circlips is limited by speeds at which pretension is relieved by centrifugal force and at which the circlip starts to lift from its seating in the groove base. In Table 1 and Table 2, detachment speed  $N_{ds}$  are given at which the circlips start to become detached from their seating in the groove (groove diameter = nominal diameter). Actual release of the circlip can be expected only after a further increase of speeds by 50%. The values apply to circlips made of spring steels as specified in 4.2.

**A-3. Shape of Groove**

**A-3.1 Groove Diameter,  $d_g$**  — The groove diameters  $d_g$  specified in 3 are selected so that the circlips are seated in the groove with pretension.

**Note** — Smaller groove diameters are possible if pretension can be dispensed. The lower limit is:

$$d_g \text{ Min} = d_g \text{ Max}$$

**A-3.2 Groove Width,  $m$**  — As a rule, for the groove width specified in Tables 1 and 2, the tolerance zone H13 applies. With unilateral power transmission, the grooves can be widened and/or chamfered towards the unloaded side. The groove width has no influence on the load-bearing capacity of the circlip connection. Intra-plant specified groove shapes and groove widths are therefore possible.

If the circlips is to be subjected to alternate power transmission on both groove edges, the groove width  $m$  shall as far as possible, for example also by reducing the tolerance, be matched to the circlip thickness,  $s$  ( for groove shapes, see Fig. 8 to 11 ).

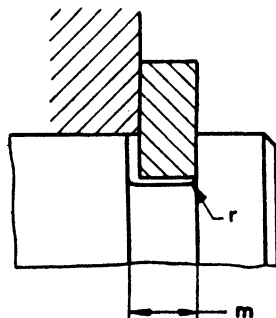


FIG. 8 GROOVE SHAPE

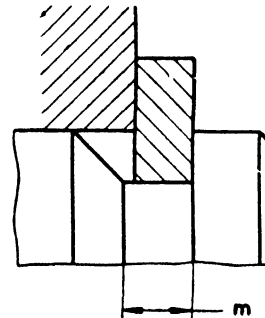


FIG. 9 GROOVE SHAPE



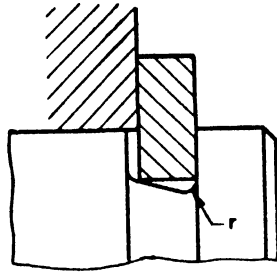


FIG. 10. GROOVE SHAPE

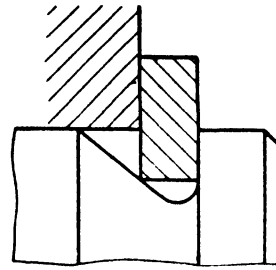


FIG. 11. GROOVE SHAPE

**A-3.3 Shape of Groove Base** — A square shape is the normal type of groove base (see Fig. 8). The radius  $r$  on the load side shall not exceed  $0.1 s$ . Other successful shapes of groove are shown in Fig. 9 to 11. In the case of a sharp-edged square groove, the notch sensitivity of the material used produces a corresponding fatigue notch factor.

#### A-4. Fitting of Circlips

**A-4.1** Pliers in accordance with IS : 7990-1976 shall preferably be used for fitting the circlips.

**A-4.1.1** When fitting, make absolutely sure that the circlips are not overspread, that is, are not opened further than is necessary for fitting over the shaft. If necessary, pliers with opening restriction (set screw) shall be used. The safest protection against overspreading is fitting with the aid of cones (see Fig. 12).

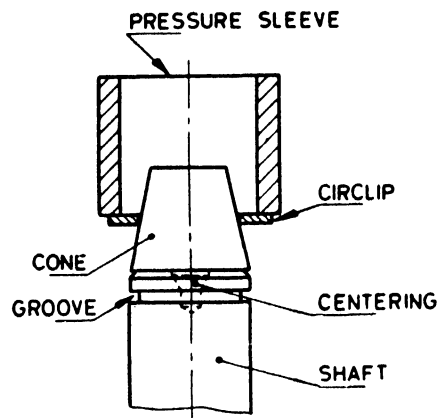


FIG. 12. FITTING WITH CONES

### EXPLANATORY NOTE

This standard was issued in 1965, as a comprehensive standard based on draft DIN 471-1963 for dimensions. Subsequently in 1981 the DIN standard was revised completely incorporating testing and acceptance requirements, but sizes and range remained the same.

The committee responsible for formulation of this Indian standard decided to revise it to bring it in line with the relevant DIN standard.

Circlips made from carbon spring steel strips or bars serve as radial spring fasteners for positioning and retaining components in assembly. Normally, the circlips are axially assembled either over shafts or inside bores.

## **IS : 3075 ( Part 1 ) - 1986**

When the circlips are assembled, a portion of the circlip protrudes from the groove to form a shoulder to support the abutting part. The part to be retained may be a ground thrust washer having a full surface contact with the shoulder providing a sharp-cornered abutment; or a ball bearing with a radiused edge which will have contact with only a portion of the shoulder; or a gear wheel with a sharpened edge which will also have contact with only a portion of the shoulder. The large corner radius or chamfer will result in a different type of assembly from that of the sharp cornered abutment.

Thus the fastening system using circlips depends on three elements, namely the circlip, the groove and the retained part. In case of axial load transmission, the circlip serves as a means of transferring the load from the retained part to the groove wall. However, in cases of impact loading, the energy absorbing capacity of the circlip will be an important factor. The more energy absorbed, the less will be transferred to the grooved wall.

Earlier standard dealt with the dimensions and other requirements for all types of circlips. In the present revision, IS : 3075-1986 has been divided into three parts to bring it in line with latest DIN standards. Testing, acceptance criteria, packaging and Standard Mark clauses have also been included.

This standard is Part 1 which covers requirements of circlips to be assembled over shaft, generally based on DIN 471-1981 'Circlips (retaining rings) for shafts — normal type and heavy type'. In addition to this, the requirements for radially assembled type of circlips, commonly known as 'E' type circlips, used for smaller shafts have been covered in part 3 of this standard. Other two parts of the standard in this series are:

**Part 2 : Specification for circlips for bores ( based on DIN 472-1981 ); and**

**Part 3 : Specification for circlips, Type E for shafts ( based on DIN 6799-1981 ).**